



# RCA MANUFACTURING COMPANY, INC.

A RADIO CORPORATION OF AMERICA SUBSIDIARY

Harrison, New Jersey

RCA RADIOTRON  
DIVISION

APPLICATION NOTE NO.67

January 20, 1937

## APPLICATION NOTE

ON

### RESISTANCE-COUPLED AUDIO-FREQUENCY AMPLIFIERS

Difficulties from low-frequency oscillation (motorboating) are often experienced when a high-gain multi-stage audio amplifier of conventional design obtains B-supply voltage from a single power-supply unit. These difficulties are usually due to interstage coupling through a common impedance in the power unit. Customary expedients to prevent motorboating include the use of very large filter condensers and several power-supply units. However, by suitable design, the gain of an audio amplifier of low frequencies can be reduced to such levels that the effects of feed-back through a power unit of conventional design are greatly reduced.

The use of a series screen resistor and a self-bias resistor offers several advantages over fixed-voltage operation: (1) the effects of possible tube differences are minimized; (2) operation over a wide range of plate-supply voltages without appreciable change in gain is feasible; and (3) the low frequency at which the amplifier cuts off is easily changed. Fixed-bias or fixed-screen-voltage operation increases the tendency of an amplifier to motorboat and decreases the compensating action of the remaining series resistors. The advantages of an amplifier constructed according to the data presented in this Note can be further emphasized by the addition of suitable decoupling resistors and condensers. With a proper decoupling filter in the plate circuit of each stage, three or more amplifier stages can be operated from a single power-supply unit of conventional design without encountering any difficulties due to coupling through the power unit; not more than two stages should be operated from a single power-supply unit when decoupling filters are not used.

Detailed information on the operation of the 2B7, 6B7, 6B8, 6C6, 6J7, and 57 as resistance-coupled audio-frequency amplifiers is presented in the accompanying Pentode Chart. These data obtain for plate-supply voltages from 45 to 600 volts, for plate-resistor values of 0.1, 0.25, and 0.5 megohm, and for a number of grid-resistor values. The combination of resistor and condenser values that is suggested in the Pentode Chart causes a 30 per cent drop in output voltage per stage at 100 cycles. A similar cut-off characteristic at any other low frequency ( $f_1$ ) can be obtained by multiplying the capacitance values shown in the chart by  $100/f_1$ .

Copyright, 1937 by  
RCA Manufacturing Co., Inc.

AN-67-1-6-37  
Printed in U.S.A.

The values of resistors and condensers suggested in the Pentode Chart were determined as follows. A cathode-ray oscilloscope was connected to show the relation between output voltage and input voltage (dynamic characteristic) of a single stage resistance-coupled amplifier. From previous experience, it is known that in an a-f amplifier employing pentode-type tubes the output voltage is substantially independent of frequency above the cut-off frequency ( $f_1$ ) and below some higher frequency ( $f_2$ ). It is also known that the value of the parallel combination of  $R_L$  and  $R_g$  determines to some extent the value of ( $f_2$ ). The following approximate values of ( $f_2$ ) obtain for the recommended values of  $R_L$  when normal circuit and tube capacitances are present.

$R_L^*$	$f_2$
0.1 megohm	20,000 cycles
0.25 "	10,000 cycles
0.5 "	5,000 cycles.

\*For the condition where  $R_L$  is less than  $R_g$ .

For given values of  $R_L$  and  $R_g$ , the magnitude of  $R_o$ ,  $R_d$ , and the input signal were adjusted until kinks just appeared at the extremities of the dynamic characteristic at the grid-current point. Under these conditions, the tube operates at the center of its dynamic characteristic, which is nearly linear throughout the operating range. Therefore, maximum output at minimum distortion is obtained. The values  $C_o$ ,  $C_d$ , and  $C$  were then determined. Very large capacitances were used in the positions indicated by  $C_o$ ,  $C_d$ , and  $C$ . The value of each was reduced, in turn, until the output voltage dropped 10 per cent at 100 cycles. Hence, for each stage of amplification, the output voltage at 100 cycles is approximately  $0.7 E_o$ , where  $E_o$  is the output voltage at some higher frequency which is less than  $f_2$ . For ( $n$ ) like stages in cascade, the output voltage at 100 cycles is  $(0.7 E_o)^n$ . For a given value of decoupling resistor, the size of the decoupling condenser can be determined in the manner similar to that used for obtaining the values of  $C_o$ ,  $C_d$ , and  $C$ .

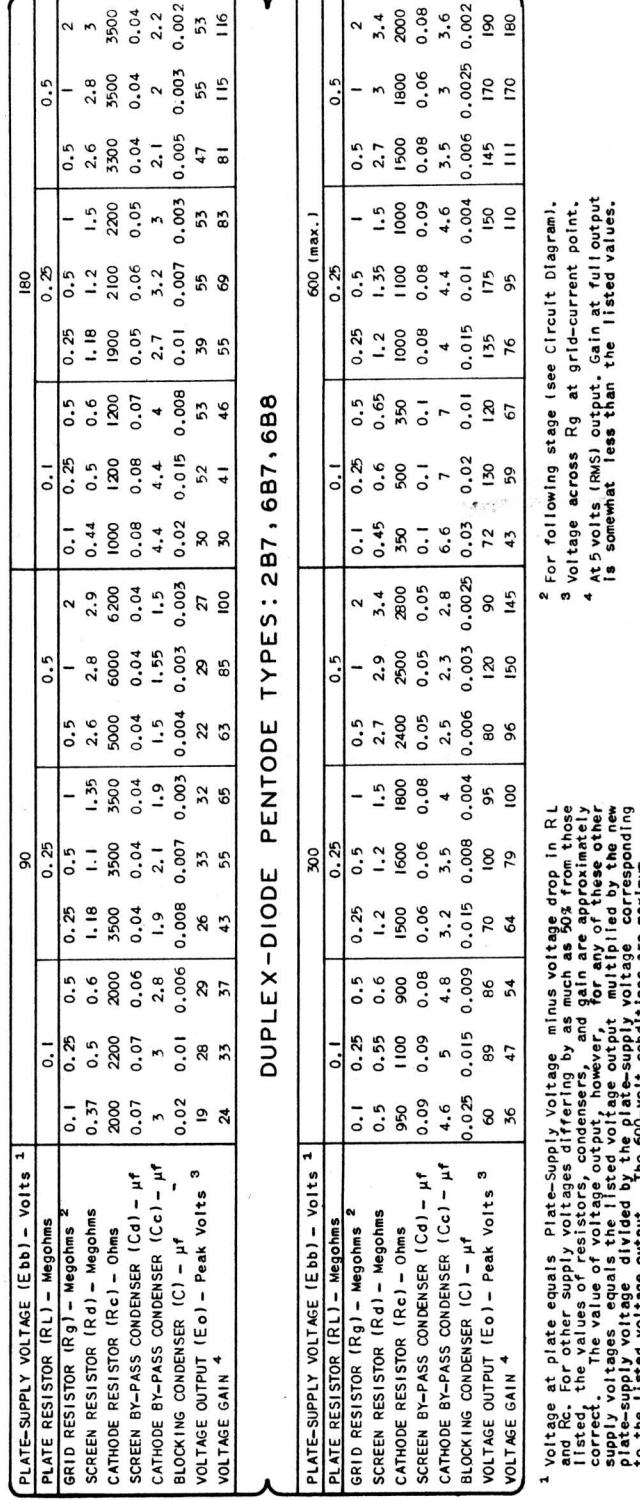
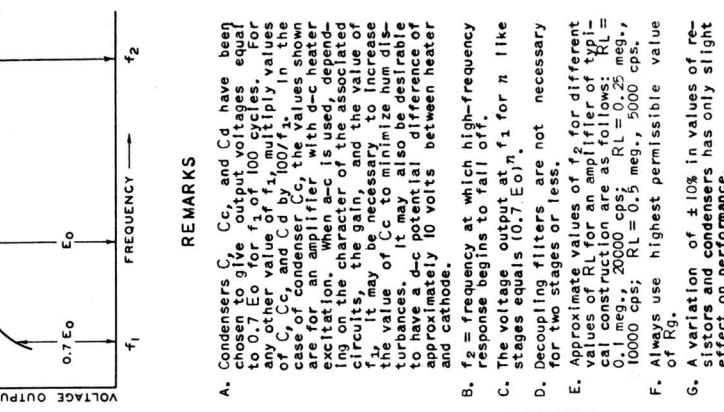
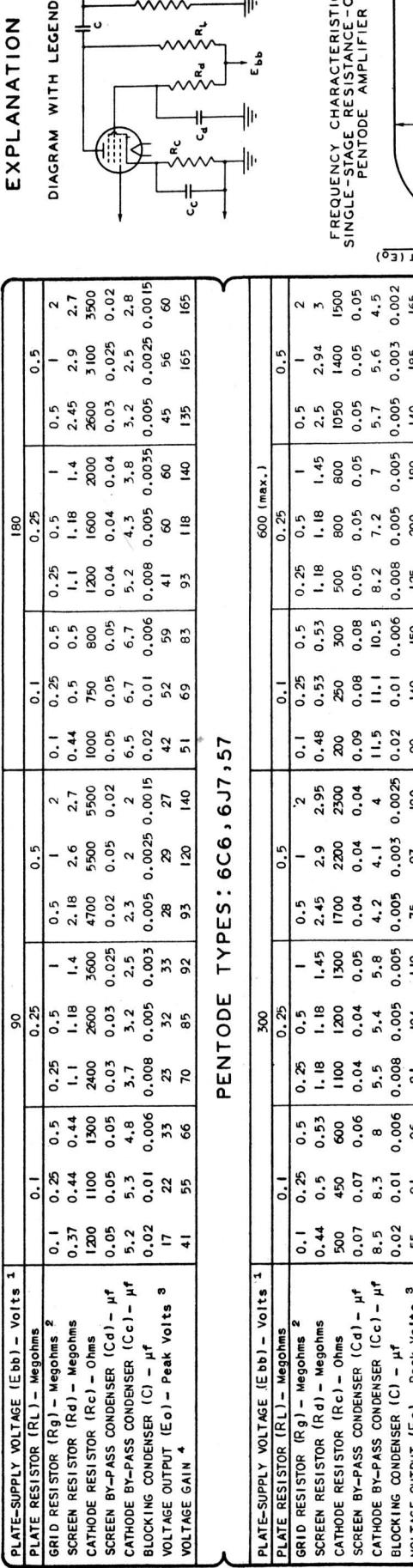
Detailed information on the operation of triodes as resistance-coupled audio-frequency amplifiers is presented in the accompanying Triode Chart. The combination of condenser and resistor values suggested in this Triode Chart causes a 20 per cent drop in output voltage per stage at 100 cycles. A similar cut-off characteristic at any other low frequency ( $f_1$ ) can be obtained by multiplying the capacitance values shown by  $100/f_1$ . As with pentodes, the use of self-bias reduces the effects of possible tube differences and permits operation over a wide range of plate-supply voltages without appreciable change in gain. The regulating action of a self-biased triode amplifier is not as good as that of a pentode amplifier having series screen and self-bias resistors, because the regulating action of a screen is not available in a triode.

When a number of high-mu triode amplifier stages are cascaded, the high-frequency response may be severely curtailed, because the high effective input capacitance of a triode shunts the load of the previous tube.

When good high-frequency response from a triode amplifier is desired, therefore, low-mu tubes and low values of plate and grid resistors should be used.

On the Charts, the values of  $C_o$  are given for an amplifier with d-c heater excitation. When a-c is used, depending on the character of the associated circuits, the gain, and the value of  $f_1$ , it may be necessary to increase the value of  $C_o$  to minimize hum disturbances. It may also be desirable to have a d-c potential difference of approximately 10 volts between heater and cathode.

# RESISTANCE-COUPLED AMPLIFIER CHART FOR PENTODES



- 1 Voltage at plate equals Plate-Supply Voltage minus voltage drop in  $R_L$  and  $R_C$ . For other supply voltages differing by as much as 50% from those listed, the values of resistors, condensers, and gain are approximately correct. The value of voltage output, however, multiplied by the new supply voltage equals the listed voltage output divided by the plate-supply voltage corresponding to the listed voltage output. The 600-volt conditions are maximum.
- 2 Always use highest permissible value of  $R_g$ .
- 3 Variation of  $\pm 10\%$  in values of resistors and condensers has only slight effect on performance.

4 A variation of  $\pm 10\%$  in values of resistors, condensers, and gain are approximately correct. The value of voltage output, however, multiplied by the new supply voltage equals the listed voltage output divided by the plate-supply voltage corresponding to the listed voltage output. The 600-volt conditions are maximum.

5 Frequency at which high-frequency response begins to fall off.

6 The voltage output at  $f_1$  for  $n$  like stages equals  $(0.7 E_o)^{1/n}$ .

7 Decoupling filters are not necessary for two stages or less.

8 Approximate values of  $f_2$  for different values of  $R_L$  and  $R_C$  construction are as follows:

- $R_L = 1000 \text{ ohms}$ ;  $R_C = 100 \text{ ohms}$ ;  $f_2 = 1000 \text{ cps}$
- $R_L = 2000 \text{ ohms}$ ;  $R_C = 200 \text{ ohms}$ ;  $f_2 = 2000 \text{ cps}$
- $R_L = 5000 \text{ ohms}$ ;  $R_C = 500 \text{ ohms}$ ;  $f_2 = 5000 \text{ cps}$

9 A variation of  $\pm 10\%$  in values of resistors and condensers has only slight effect on performance.

# RESISTANCE-COUPLED AMPLIFIER CHART FOR TRIODES

$C_b$  = BLOCKING CONDENSER ( $\mu F$ )       $C_d$  = SCREEN BY-PASS CONDENSER ( $\mu F$ )       $E_o$  = VOLTAGE OUTPUT (Peak Volts)  
 $C_c$  = CATHODE BY-PASS CONDENSER ( $\mu F$ )       $E_{bb}$  = PLATE-SUPPLY VOLTAGE (Volts)       $R_d$  = SCREEN RESISTOR (Megohms)  
 $R_c$  = CATHODE RESISTOR (Ohms)       $R_g$  = GRID RESISTOR (Ohms)       $V.G.$  = VOLTAGE GAIN

$R_L$  = PLATE RESISTOR (Megohms)       $R_g$  = GRID RESISTOR (Megohms)  
 $V.G.$  = VOLTAGE GAIN

TRIODE TYPES : 2A6, 75

		90										180										300														
		0.25					0.5					0.1					0.25					0.5					0.1					0.25				
Ebb 1		RL	0.1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.5	1	2
Rg	2	0.1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.5	1	2	
Rc	6300	6600	6700	10000	11000	15000	16200	16600	17400	2600	2900	3000	4300	4800	5300	7000	8000	10000	2200	2300	3300	3900	4200	5300	6100	7000	Rg	2	Rc	Cc	Eo	V.G.	4			
Cc	2.2	1.7	1.7	1.24	1.07	0.9	0.75	0.7	0.65	3.3	2.9	2.7	2.1	1.8	1.5	1.3	1.1	0.9	4	3.5	3	2.7	2	1.8	1.6	1.3	1.2	Cc	3	Eo	3	V.G.	4			
C	0.02	0.01	0.006	0.01	0.006	0.003	0.005	0.003	0.0015	0.025	0.015	0.007	0.015	0.004	0.007	0.004	0.002	0.03	0.015	0.007	0.015	0.007	0.004	0.007	0.004	0.002	C	3	Eo	3	V.G.	4				
Eo	3	5	6	5	7	10	7	10	13	16	22	23	21	28	33	38	31	41	45	42	51	60	47	62	67	60	63	Eo	3	V.G.	4					
V.G.	4	25	d	29	b	31	c	34	b	40	c	40	39	44	48	29	36	37	43	50	53	52	57	31	39	42	48	53	56	V.G.	4					

TRIODE TYPE 6F5

		90										180										300														
		0.25					0.5					0.1					0.25					0.5					0.1					0.25				
Ebb 1		RL	0.1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.5	1	2
Rg	2	0.1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.5	1	2	
Rc	4400	4800	5000	8000	9000	12200	13500	14700	1800	2000	2200	3500	4100	4500	6100	6900	7700	1300	1600	1700	2600	3200	3500	4500	5400	6100	Rc	2	Rc	Cc	Eo	V.G.	4			
Cc	2.5	2.1	1.8	1.33	1.18	0.9	0.76	0.67	0.58	4.4	3.3	2.9	2.3	1.8	1.7	1.3	0.9	0.83	5	3.7	3.2	2.5	2.1	2	1.5	1.2	0.93	Cc	3	Eo	3	V.G.	4			
C	0.02	0.01	0.005	0.01	0.005	0.003	0.006	0.005	0.0015	0.025	0.015	0.006	0.01	0.006	0.01	0.006	0.003	0.0015	0.025	0.01	0.006	0.01	0.007	0.004	0.006	0.002	C	3	Eo	3	V.G.	4				
Eo	3	4	5	6	6	7	10	8	10	12	16	23	25	21	16	23	25	21	26	32	24	33	37	43	48	51	53	63	66	62	70	V.G.	4			
V.G.	4	28	d	34	b	35	c	39	b	43	c	44	43	46	48	37	44	46	44	52	57	53	57	57	53	57	53	57	57	63	67	65	V.G.	4		

TWIN-TRIODE TYPES: 6A6, 6N7, 53 (ONE TRIODE UNIT)

		90										180										300																			
		0.25					0.5					0.1					0.25					0.5					0.1					0.25									
Ebb 1		RL	0.1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.5	1	2					
Rg	2	0.1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.25	0.5	1	0.5	1	2	0.1	0.25	0.5	1	0.5	1	2						
Rc	2050	2200	2350	4000	4250	4650	6150	6850	7500	11000	15100	18300	2400	3000	3700	4500	6500	7600	10700	14700	17700	2400	3100	3800	4500	6400	7500	11000	15200	18500	Rc	2	Rc	Cc	Eo	V.G.	4				
Cc	2	1.6	1.25	1.05	0.82	0.68	0.48	0.36	0.32	2.5	1.9	1.65	1.45	0.97	0.8	0.6	0.45	0.4	2.8	2.2	1.8	1.6	1.2	0.98	0.69	0.5	0.4	Cc	3	Eo	3	V.G.	4								
C	0.06	0.03	0.015	0.03	0.015	0.015	0.015	0.007	0.0035	0.06	0.035	0.015	0.035	0.015	0.035	0.015	0.035	0.015	0.045	0.015	0.045	0.015	0.045	0.015	0.045	0.015	0.045	0.015	0.045	0.015	0.045	0.015	0.045	0.015	V.G.	4					
Eo	3	16	21	23	19	23	25	21	24	28	36	40	34	38	40	42	41	42	44	42	44	41	42	34	37	41	42	44	45	49	53	57	61	67	71	75	82	96	108	V.G.	4
V.G.	4	7	7.7	8.1	8.1	8.9	9.3	9.4	9.7	9.8	7.7	8.2	9	9.3	9.4	9.7	10	10	8.3	8.9	9.4	9.5	9.7	10	10	10	10	10	10	10	10	10	10	10	10	10	10	V.G.	4		

TWIN-TRIODE TYPE 79 (ONE TRIODE UNIT)

		90										180										300														
		0.25					0.5					0.1					0.25					0.5					0.1					0.25				
Ebb 1		RL	0.1	0.25	0.5	1</																														

(continued from preceding page)

TYPES: 6C5 (TRIODE), AND 6C6, 6J7, 57 (AS TRIODES)

DUPLEX-DIODE TRIODE TYPE 6Q7

Ebb 1	90					180					300					Ebb 2							
	0.1	0.25	0.5	0.75	1	0.1	0.25	0.5	0.75	1	0.1	0.25	0.5	0.75	1								
RL	Rg	Rc	Cc	Cc	RL	Rg	Rc	Cc	Cc	RL	Rg	Rc	Cc	Cc	RL								
4000	4200	4500	4700	5000	11500	12500	13700	16000	19000	21000	34000	40000	45000	60000	15000	17000	25000	30000	36000	46000	55000	62000	
2.07	1.7	1.5	1.2	1.0	0.9	0.72	0.6	0.45	0.3	2.5	2.3	1.6	1.3	1.05	0.86	0.76	0.65	4.4	3.6	2.4	1.66	1.45	1.2
0.02	0.01	0.005	0.01	0.006	0.003	0.003	0.003	0.006	0.005	0.02	0.01	0.005	0.005	0.003	0.003	0.003	0.003	0.015	0.015	0.007	0.007	0.004	0.002
5	8	9	11	13	9	13	17	19	26	29	25	31	37	30	36	41	52	53	43	52	47	60	66
23 a	28 b	29 c	31 b	33	31	33	37	33	35	36	38	40	41	34	39	40	42	45	45	46	47	V.G. 4	V.G. 4

DUPLEX-DIODE TRIODE TYPE 6R7

Ebb 1		Ebb 2		Ebb 3		Ebb 4	
RL	0.05	RL	0.05	RL	0.05	RL	0.05
Rg 2	0.05	Rg 2	0.1	Rg 2	0.1	Rg 2	0.1
Rc	0.05	Rc	0.1	Rc	0.1	Rc	0.1
Cc	0.05	Cc	0.1	Cc	0.1	Cc	0.1
Eo 3	0.05	Eo 3	0.1	Eo 3	0.1	Eo 3	0.1
V.G. 4	0.05	V.G. 4	0.1	V.G. 4	0.1	V.G. 4	0.1
90							
0.1	0.25	0.5	0.25	0.5	0.1	0.25	0.5
0.25	0.5	1	0.05	0.1	0.1	0.25	0.5
0.5	1	1	0.05	0.1	0.1	0.25	0.5
1	1	1	0.05	0.1	0.1	0.25	0.5
2.5	5.0	10.0	2.5	5.0	1.0	2.5	5.0
5.0	10.0	20.0	5.0	10.0	2.0	5.0	10.0
10.0	20.0	40.0	10.0	20.0	4.0	10.0	20.0
180							
0.1	0.25	0.5	0.1	0.25	0.5	0.1	0.25
0.25	0.5	1	0.05	0.1	0.1	0.25	0.5
0.5	1	1	0.05	0.1	0.1	0.25	0.5
1	1	1	0.05	0.1	0.1	0.25	0.5
2.5	5.0	10.0	2.5	5.0	1.0	2.5	5.0
5.0	10.0	20.0	5.0	10.0	2.0	5.0	10.0
10.0	20.0	40.0	10.0	20.0	4.0	10.0	20.0
300							
0.1	0.25	0.5	0.1	0.25	0.5	0.1	0.25
0.25	0.5	1	0.05	0.1	0.1	0.25	0.5
0.5	1	1	0.05	0.1	0.1	0.25	0.5
1	1	1	0.05	0.1	0.1	0.25	0.5
2.5	5.0	10.0	2.5	5.0	1.0	2.5	5.0
5.0	10.0	20.0	5.0	10.0	2.0	5.0	10.0
10.0	20.0	40.0	10.0	20.0	4.0	10.0	20.0

DUPLEX-DIODE TRIODE TYPES: 55, 85

<sup>1</sup> Voltage at plate equals Plate-Supply Voltage minus voltage drop in  $R_L$  and  $R_C$ . For other supply voltages differing by as much as 50% from those listed, the values of resistors, condensers, and gain are approximately correct. The value of voltage output, however, for any of these other supply voltages, equals the listed voltage output multiplied by the new plate-supply voltage divided by the plate-supply voltage corresponding to the listed voltages.

- Voltage across  $R_g$  at grid-current point.
- Voltage Gain at 5 volts (RMS) output unless

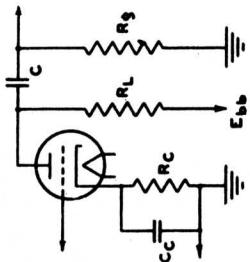
C At 4 volts (RMS) output.

d At 2.2 volts (RMS) output

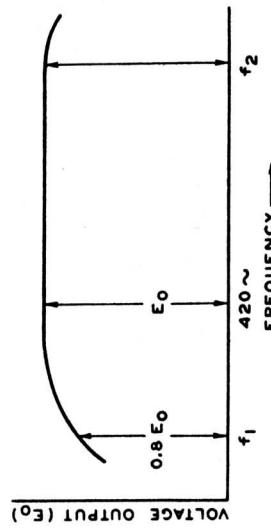
הנִזְמָן

See next page for Diagrams and Notes.

TRIODE DIAGRAM WITH LEGEND



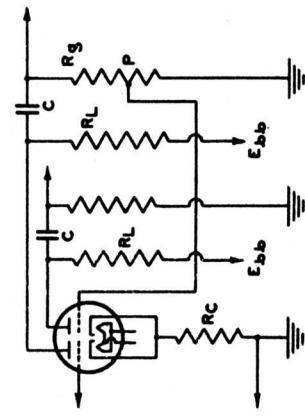
FREQUENCY CHARACTERISTIC OF  
SINGLE-STAGE RESISTANCE-COUPLED  
TRIODE AMPLIFIER



NOTES

- A. Condensers C and Cc have been chosen to give output voltages equal to 0.8 Eo for f1 of 100 cycles. For any other value of f1, multiply values of C and Cc by 100/f1.
- In the case of condenser Cc, the values shown are for an amplifier with d-c heater excitation. When a-c is used, depending on the character of the associated circuits, the gain, and the value of f1, it may be necessary to increase the value of Cc to minimize hum disturbances. It may also be desirable to have a d-c potential difference of approximately 10 volts between heater and cathode.
- B. f2 = frequency at which high-frequency response begins to fall off.
- C. The voltage output at f1 for n like stages equals (0.8 Eo)<sup>n</sup>.

TWIN-TRIODE DIAGRAM WITH LEGEND



FREQUENCY CHARACTERISTIC OF  
RESISTANCE-COUPLED  
TWIN-TRIODE AMPLIFIER

SEE INFORMATION UNDER TRIODE AMPLIFIER WHICH IN  
GENERAL APPLIES ALSO TO THIS CASE.

NOTES

- The diagram given above is for Phase-Inverter Service. The signal input is supplied to the grid of the left-hand triode unit. The grid of the right-hand unit obtains its signal from a tap (P) on the grid resistor (Rg) in the output circuit of the left-hand triode unit. The tap (P) is chosen so as to make the voltage output of the right-hand unit equal to that of the left-hand unit. Its location is determined from the voltage gain values given in the Chart. For example, if the value of voltage gain is 20 (from the Chart), (P) is chosen so as to supply 1/20 of the voltage across (Rg) to the grid of the right-hand triode.
- For phase-inverter service, the cathode resistor (Rc) should not be by-passed by a condenser. Omission of the condenser in this service assists in balancing the output voltages. The value of (Rc) is specified on the basis that both units are operating simultaneously at the same values of plate load and plate voltage.



**RCA MANUFACTURING COMPANY, INC.**

A RADIO CORPORATION OF AMERICA SUBSIDIARY

*Harrison, New Jersey*

**RCA RADIOTRON**  
D I V I S I O N

**EXPLANATION OF TWIN-TRIODE  $R_o$  VALUES**

**APPLICATION NOTE No. 67  
ON  
RESISTANCE-COUPLED AUDIO-FREQUENCY AMPLIFIERS**

In the Triode Chart of this Note, it should be observed, as stated in Notes under Twin-Triode Diagram, that the  $R_o$  values for Twin-Triode types 6A6, 6N7, 53, and 79 are for two triode units on basis that tube type is used in phase-inverter service. Other tabulated data on these types are given for each triode unit.